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The radius of a tube is determined of the permissible temperature drop across the tube section.

When a tube is designed for a reactor with a granular bed of catalyst, then the permissible temperature drop across the tube section determines the radius. The temperature profile across a tube section is, in the case of a zeroth-order reaction, analogous to that in [1]:

$$\pm \theta = \ln \frac{8}{\delta \left[\exp \left(-\mu \right) \rho^2 \pm \exp \mu \right]^2},\tag{1}$$

where $\exp(-\mu) = \sqrt{\sigma}$, and σ are the roots of the characteristic equation

$$\frac{8\sigma}{\delta (\sigma \pm 1)^2} = \exp \frac{4\sigma}{\mathrm{Bi}(\sigma \pm 1)}.$$
 (2)

Here and later on the upper sign refers to an exothermal reaction, the lower sign refers to an endothermal reaction.

The method proposed in [1] is convenient to use for determining the permissible tube radius on the basis of the given temperature drop from the center to the wall. From expression (1) we have

$$\Delta \theta = |\theta_{\mathbf{c}} - \theta_{\mathbf{w}}| = 2 \ln (\sigma \pm 1), \tag{3}$$

$$\sigma = \exp\left(\Delta\theta/2\right) \equiv 1. \tag{4}$$

For stipulated values of $\Delta\theta$ one determines the permissible value of the Biot number from the solution to the equation

$$c \operatorname{Bi}^{2} - \frac{8\sigma \exp\left[-\frac{4\sigma}{\operatorname{Bi}(\sigma \pm 1)}\right]}{(\sigma \pm 1)^{2}} = 0,$$
 (5)

where $c = |h|Ek\lambda_{eff}/R(T_{\alpha}\alpha)^2$.

From this Bi one then determines the permissible tube radius

$$r_0 = \text{Bi}\lambda_{\text{eff}}/\alpha$$
.

It is to be noted that Eq. (5) has no solution when

$$\sigma c \gg 2 \exp(-2) = 0.270671$$
 (6)

or

$$Bi_{cr} < \frac{2\sigma}{\sigma \pm 1}. \tag{7}$$

In this case the stipulated temperature drop cannot be realized, regardless of the tube radius.

For real values of all parameters $\Delta\theta$ lies within 0-30. The calculations of Bi_{Cr} as a function of $\Delta\theta$ are shown in Fig. 1.

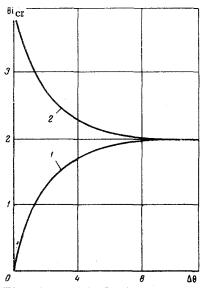


Fig. 1. Critical Biot number Bi_{Cr} as a function of the temperature drop $\Delta\theta$: 1) exothermal reaction; 2) endothermal reaction.

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Characteristically, it is not possible to realize a zero temperature drop during an exothermal reaction. The maximum tube radius corresponds to small temperature drops during endothermal reactions, while $\mathrm{Bi}_{\mathrm{Cr}} < 4$. When the temperature drop is large ($\Delta \theta > 10$), then $\mathrm{Bi}_{\mathrm{Cr}} = 2$ for both exothermal and endothermal reactions.

NOTATION

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is the local absolute temperature at a tube section;
\mathbf{T}
T_{\mathbf{c}}
                                                    is the temperature at the tube axis;
                                                   is the temperature at the tube wall;
T_{\mathbf{w}}
                                                    is the ambient temperature;
k = k_0 \exp(-E/RT_a)
                                                    is the rate constant of the reaction;
\mathbf{k_0}
                                                    is the cofactor of the exponential term in the rate constant;
                                                   is the thermal effect of the reaction;
h
                                                   is the universal gas constant;
\mathbf{R}
                                                    is the activation energy of the reaction;
\mathbf{E}
r
                                                    is the local radius;
                                                    is the inside radius of the tube;
                                                    is the dimensionless local radius;
\rho = \mathbf{r}/\mathbf{r}_0
                                                    is the effective radial thermal conductivity of the granular bed;
\lambda_{eff}
                                                    is the coefficient of heat transfer from bed to coolant;
\theta = E(T - T_a) / RT_a^2;
\delta = \ln |\text{Ekr}_0^2/\lambda_{\text{eff}} R T_0^2
                                                    is the heat source (sink) parameter;
                                                    are the roots of the characteristic equation (2);
Bi = \alpha r_0 / \lambda_{eff};
                                                    is the Biot number;
\theta_{c} = E (T_{c} - T_{a}) / R T_{a}^{2};

\theta_{w} = E (T_{w} - T_{a}) / R T_{a}^{2}.
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LITERATURE CITED

1. A. G. Gorelik, Inzh. Fiz. Zh., 21, No. 2, 265 (1971).